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A Study of the Origin of Organic Pollutants in Fossil Fuel Production _ Part II Interruption and Modification of Pollutant Pathways

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中文摘要:

在論文的第一部份中,有機污染物的生成和根源已以地質化學和石油化學的觀點探討過。在此第二部份中,有關於改良或打消這些有機污染物的方法則被廣泛的討論。這些方法包括制止反應進行、添加物法、前後期處理、和單元操作上的改良。

Abstracts:

In part I of this paper, the genesis and origin of organic pollut-ants from the geochmical and petrochemical points of view are already discussed. In part II, ways to interrupt or modify pollutant formation during processing by quenching, addition of additives, reaction blocking pretreatment, post-treatment or designed-modification are introduced.

1. Introduction:

In order to be consistent with the definition of pollutants, in the previously discussed Equation 1 through 4, the pollutant species may be exgressed by ji, where j = 1, 2, 3, 4. In this manner a copollutant can be 3_i or 4_i . For example, when phenolics react with ammonia, heteroyclic systems containing nitrogen may form. The Bremner-Flaig sequences (1) are illustrated in Table 1. This type of reaction indicates a possible pathway of nitrogeneous heterocyclic formation in oil shale production.

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Coames (2) and Epler et al. (3) showed that for oil shale materials, carcinogenicity decreased with decreasing nitrogen content. Rao et al. (4) showed that for shale oil fractions, the neutral and basic fractions were responsible for the mutagenicity. The basic and neutral fractions of retort water were shown to be refractoric foward biodegradation, especially the nitrogeneous compounds (5). For this reason, any formation mechanism which led to nitrogen heterocyclics should be blocked as much as possible. One practical approach is to set up an ammonia trap so that the ammonic reaction cannot proceed. There are many methods to eliminate or reduce ammonia concentration, e.g., stripping, ion exchange, neutralization, and application of vacuum, etc.

2. Application of Additives:

An important (traditional) additive for shale oil is a pour point depressor that renders it transportable (6). A serious problem with synthetic fuels is the inferiority of the storage stability and the thermal (high temporature) stability. In both cases the oil will deposit enough gum to cause trouble. To meet this need, antioxidants such as phenylene diamine or a hindered phenol (e.g., 2,6-di-t-buty1-4methy1 phenol) are added to shale oils and coal liquids (6).

Brinkman et al. (7) stated that the more severe the level of hydrotreating, the more stable the fuel. They found that the polyalkyl pyrroles are strongly deleterious, and the parent heterocyclics are relatively harmless. A plausible mechanism is the polycondensation through the two α -positions, e.g.,

At any rate, the direct scientific input is useful for the process design modification in such a way that will benefit the control strategy. For example, we know that the basic solid surface of CaO and/or CaO/Al₂O₃ or MgO-Fe₃O₃-K₂O system is very efficient for converting a number of alkyl benzenes into styrene and causes extensive polymerization.

The oil shale matrix and spent shale components contain the same basic catalyts. It is possible that extensive catalytic conversion of alkyl benzenes and the copolymerization with the alkenes isolated occur. Experimental observation of a larger oil yield, using the carbonatefree oil shale, and the fact that the delayed coking process yields a large proportion of carbon, tends to support this fact.

Indeed, a fluidized-bed concept for the retorting (23) would solve this problem of excessive carbon formed. In addition the ring cyclization of alkyl pyrrole may be avoidable due to the short contact or residence time. The recent shell pellet heat exchange retorting (SPHER) (24) may have some of these advantages.

5. Conculsion:

In the above analysis, the ways to interrupt or modify pollutant formation

during processing are already pointed out breifly. However, much basic information is needed in order to reassess the design criterion of a new breed of system which combine the engineering process and production and the technology of environmental control. For example, in measuring the thermal (high temperature) stability of synthetic fuels, the method such as the spin concentration (Ng) vs. temperature profile by ESR should be developed (26). Finally, but not the last, I want to thank Dr. Teh-Fu Yen of University of Southern California for his many kindly suggestions on the above work.

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OH \\
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Table 1. Ammonia Reactions with Phenolics (from Yen and Tang, Ref. 25).

TABLE 2. A Summary or the Chemical Desulfurization Processes *Source, Deurbrouck, Ref. 8.

	ARCO							e di Ville		mog sá	Labora- tory
	A	Two- stage cheml- eal oxida-	tion					40			Labor
24	GE	Micro- wave caustic leach	H ₂ O, N _a OH	Atmos- pheric		95					Bench scale
	KVB	Dry oxidation	02, N2,NO H2O. N2OH	15-300	40-260 1	06		Up to 40		Gypsum	Inactive
	JPL	Chlorine/ water leach	Cl., H ₂ O, CH ₃ CO,	Atmos- pheric	65-05 2-4	06		Up to 50		H ₂ SO ₄	Bench scale
	PERC	Air water leach	Air, H ₂ O,, lime	500-1500	150-200	06		Up to 40		Gypsum	Bench scalede-sign of continuous unit
	t Ames	Oxygen/ sodium cabonate leach	O2, H2O, Na2CO3, Ijme	0-1000	10-230	06		Up to 25		Gypsum	Bench scale
	Ledgemont	Oxygen/ ammonia leach	O2, H2O, NH3, lime	0-1000	10^{-230} $1/4-24$	06		Up to 25		Cypsum	Inactive
	Battelle	- Caustic cal Pre-treatment plus magnetic separation	Ca(OH), H ₂ O, CO ₂	350-2,500	1/4-1/2	06		Up to 40 Up to 25		H ₂ S, elemental sulfur	Pilot unit, 0.25 ton/year
	Magnex	Acid leach Dry chemi-	Fe(CO);	Atmos- pheric	1/10-1	06		2 L 0		Dry sulfurous mineral matter	Pilot unit, 200 lb/day
The state of the s	TRW	Acid leach	Fe, $(SO_4)_3$, $H_2O_2O_2$, acetone	15-80° - 90-135	1/2-10	06		0		Iron sulfates, elemental sulfur	Pilot plant, 8 tons/day
	Process	Method	Reagent(s)	Pressure (psia) Temperature	(°C) Retention 1/2-10	(hr) $\mathrm{Pyritie}_{1}$	sulfur reduction (%)	Organic sulfur re-	(%)	Sulfur product	Status